

Optimal Deployment of Mobile Sensors for Target Tracking in 2D and 3D Spaces

Shiyu Zhao Ben M Chen Tong H Lee

Abstract—This paper proposes a control strategy to autonomously deploy optimal placements of range-only mobile sensors in 2D and 3D spaces. Based on artificial potential approaches, the control strategy is designed to minimize the inter-sensor and external potentials. The inter-sensor potential is the objective function for optimal sensor placements. A placement is optimal when the inter-sensor potential is minimized. The external potential is introduced to fulfill constraints on sensor trajectories. Since artificial potential approaches can handle various issues such as obstacle avoidance and collision avoidance among sensors, the proposed control strategy provides a flexible solution to practical autonomous optimal sensor deployment. The control strategy is applied to several optimal sensor deployment problems in 2D and 3D spaces. Simulation results illustrate how the proposed control strategy can improve target tracking performance.

Index Terms—Optimal sensor placement, mobile sensor network, artificial potential, target tracking.

I. INTRODUCTION

FOR target tracking using mobile sensor networks, the placement of the sensors relative to the target can significantly affect the tracking performance. What is the optimal sensor placement that can minimize target tracking uncertainty? This problem is of both theoretical and practical importance.

There are generally two kinds of mathematical formulations for optimal sensor placement problems in the literature: one is optimal control^[1–3], and the other is parameter optimization^[4–11]. The optimal control formulation considers sensor placement and target tracking as a whole. The formulation is also referred to simultaneous localization and planning (SLAP)^[2]. As a comparison, the parameter optimization formulation only considers the sensor placement part and does not consider the target tracking part. It is assumed that an initial target estimate has already been obtained in other ways. Then the optimal sensor placement is determined based on this initial target estimate. In fact, the above two kinds of formulations lead to consistent results. For example, the work in [2] observed that when two sensors approach a target, the target information would be maximized when the angle subtended at the target by the two sensors is 90 deg. This observation actually has been analytically proved as an optimality condition based on the parameter optimization formulation in [4, 6–7, 13–14]. It should be noted that analytical conclusions

can be drawn based on the parameter optimization formulation, while only numerical results can be obtained from the optimal control formulation. Considering the analytical conclusions can provide us important insights into the effects of sensor placements on target tracking, we will adopt the parameter optimization formulation to study optimal sensor placement in this paper.

Although optimal sensor placement based on the parameter optimization formulation has been investigated extensively, most of the existing results are only applicable to 2D cases^[4–8, 10]. Since many practical applications require 3D optimal sensor placements, the general results for 3D cases will be of great importance from the practical point of view. One main difficulty to analyze 3D optimal placements is that the complexity of the conventional objective function, the determinant of the Fisher information matrix (FIM), increases dramatically as the dimension increases from two to three. Motivated by that, a new objective function, which is analytically tractable in both 2D and 3D cases, has been proposed in [13]. By employing recently developed frame theory, the work in [13] successfully proved the necessary and sufficient conditions of optimal sensor placements in both 2D and 3D spaces. It is shown that the analytical results obtained based on the new objective function are consistent with the existing 2D results in the literature. Moreover, the work in [13] proposed a unified framework for analyzing the optimal placement problems of bearing-only, range-only and received-signal-strength sensor networks.

In addition to analytically determining optimal sensor placements, it is also practically important to study how to autonomously deploy the optimal placements. There are generally three approaches to autonomous optimal sensor deployment. 1) One approach is to use the optimal control formulation mentioned above. 2) The second approach is to develop numerical methods to solve the parameter optimization formulation. For example, by numerically maximizing the determinant of the FIM, sensor trajectory optimization algorithms can be obtained^[3, 9]. Compared to the optimal control approach, the second one is easy to be designed and implemented, and various constraints of sensor trajectories can be easily included. 3) The third approach is to design autonomous deployment algorithms based directly on analytical results of optimal sensor placement. For example, the work in [7] proposed a distributed motion coordination algorithm to autonomously deploy sensors for target tracking. Loosely speaking, that algorithm is designed based on the fact that a placement is optimal if range-only sensors are uniformly distributed around the target. However, one limitation of the approach used in [7] is that the uniformly distributed placement is merely a special case as pointed out by [13, Section 5.2]. There are an infinite number of optimal

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placements that can optimize the objective function. These optimal placements may be more appropriate than the uniformly distributed one given certain initial placements and sensor trajectory constraints. More importantly, the uniformly distributed placement is optimal only if the sensors are equally weighted [13, Section 5.2]. If some of the sensors can provide more accurate measurements than the others, the uniformly distributed one will no longer be optimal. With the above analysis, we will adopt the second numerical optimization approach to solve autonomous sensor deployment problems in this paper.

Based on the analytical results in [13], this work proposes a control strategy to autonomously deploy optimal placements of range-only sensors in 2D and 3D spaces. One main contribution of this work is that the control strategy can handle 3D autonomous deployment problems while the existing results are only applicable to 2D cases^[1-3, 7, 9]. The objective function to be minimized is composed of two terms: an inter-sensor potential and an external potential. The inter-sensor potential actually is the frame potential among the sensors^[13]; the sensor trajectory constraints are formulated as the external potential. A gradient control law is used to numerically to minimize the objective function such that an optimal placement can be achieved while the sensor trajectory constraints can be satisfied in the meantime. Since artificial potential approaches can handle various issues such as obstacle avoidance and collision avoidance among sensors, the proposed control strategy provides a flexible solution to practical autonomous optimal sensor deployment problems. In this paper, we further apply the control strategy to several specific scenarios. Simulation results verify the effectiveness of the proposed control strategy. It is also illustrated how the control strategy can improve target tracking performance.

II. OPTIMAL SENSOR PLACEMENT

Consider one target in \mathbf{R}^d where $d = 2$ or 3 . Suppose there are n ($n \geq d$) range-only sensors. Following the existing work [4–7], we assume an initial target position estimate $p \in \mathbf{R}^d$ is available already. The optimal placement will be determined based on p . Denote $s_i \in \mathbf{R}^d$ as the position of sensor i ($i \in \{1, \dots, n\}$). The relative position of sensor i with respect to the target is $r_i = s_i - p$. Then $\{r_i\}_{i=1}^n$ can fully describe the sensor-target placement. The unit vector

$$g_i = \frac{r_i}{\|r_i\|}$$

represents the bearing of sensor i relative to the target, where $\|\cdot\|$ denotes the Euclidean norm of a vector or the Frobenius norm of a matrix. The above notations are illustrated by Fig. 1.

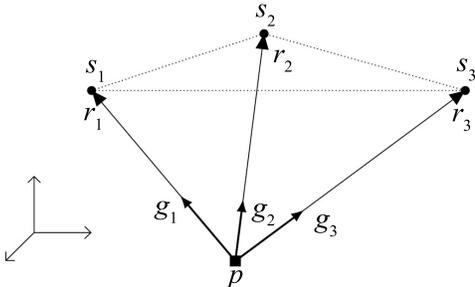


Fig. 1. A 3D sensor placement.

The measurement model of sensor i is expressed as

$$m_i = h_i(p) + w_i,$$

where

$$h_i(p) = \|p - s_i\|, \quad (1)$$

and $m_i \in \mathbf{R}$ is the measurement corrupted by noise $w_i \in \mathbf{R}$. We assume w_i to be a zero-mean Gaussian noise with standard deviation as σ_i . By further assuming the measurement noises of different sensors are uncorrelated, the FIM given by n sensors is expressed as

$$F = \sum_{i=1}^n \left(\frac{\partial h_i}{\partial p} \right)^T \Sigma_i^{-1} \frac{\partial h_i}{\partial p}, \quad (2)$$

where $\frac{\partial h_i}{\partial p}$ denotes the Jacobian of $h_i(p)$ with respect to p . We refer to [4, Section 3] for a detailed derivation of the FIM formula in (2). Substituting (1) into (2) yields

$$F = \sum_{i=1}^n c_i^2 g_i g_i^T, \quad (3)$$

where $c_i = 1/\sigma_i$. Note we do not assume different sensors have the same noise level. Instead, σ_i can be an arbitrary positive constant.

The conventional optimization criterion for optimal sensor placement is to maximize $\det F$, which can be interpreted as maximizing the target information obtained by the sensors. This criterion, however, is not applicable to 3D cases as $\det F$ is not analytically tractable in 3D cases. Motivated by that, the work in [13] proposed a new objective function. Let $\{\lambda_i\}_{i=1}^d$ be the eigenvalues of F . Denote $\bar{\lambda} = 1/d \sum_{i=1}^d \lambda_i$. Since $\sum_{i=1}^d \lambda_i = \text{tr} F$, it is easy to obtain $\bar{\lambda} = 1/d \sum_{i=1}^d c_i^2$. The new objective function is defined as $\|F - \bar{\lambda} I_d\|^2$, where $I_d \in \mathbf{R}^{d \times d}$ is the identity matrix. Minimizing $\|F - \bar{\lambda} I_d\|^2$ is to minimize the diversity of the eigenvalues of F . A detailed discussion on the relationship between the new and the conventional objective functions is given in [13, Section 3.2].

A sensor placement is called optimal if it minimizes the objective function $\|F - \bar{\lambda} I_d\|^2$. By [13, Lemma 3.3], a placement is optimal if and only if it minimizes $\|G\|^2$, where

$$G = \sum_{i=1}^n c_i^2 g_i g_i^T.$$

By employing recently developed frame theory^[15], necessary and sufficient conditions of optimal placements that minimize $\|G\|^2$ are obtained as below^[13].

Definition 1 (Irregularity). For any positive non-increasing sequence $\{c_i\}_{i=1}^n$ with $c_1 \geq \dots \geq c_n > 0$, and any integer d satisfying $1 \leq d \leq n$, denote k_0 as the smallest nonnegative integer k for which

$$c_{k+1}^2 \leq \frac{1}{d-k} \sum_{i=k+1}^n c_i^2.$$

The integer k_0 is called the irregularity of $\{c_i\}_{i=1}^n$ with respect to d . If $k_0 = 0$, the sequence $\{c_i\}_{i=1}^n$ is called regular; otherwise, it is called irregular.

Theorem 1 (Regular optimal placement). In \mathbf{R}^d with $d = 2$ or 3 , if the positive coefficient sequence $\{c_i\}_{i=1}^n$ is regular, then the objective function $\|G\|^2$ satisfies

$$\|G\|^2 \geq \frac{1}{d} \left(\sum_{i=1}^n c_i^2 \right)^2. \quad (4)$$

The lower bound of $\|G\|^2$ is achieved if and only if

$$\sum_{i=1}^n c_i^2 g_i g_i^T = \frac{1}{d} \sum_{i=1}^n c_i^2 I_d. \quad (5)$$

Theorem 2 (Irregular optimal placement). In \mathbf{R}^d with $d = 2$ or 3 , if the positive coefficient sequence $\{c_i\}_{i=1}^n$ is irregular with irregularity as $k_0 \geq 1$, without loss of generality, $\{c_i\}_{i=1}^n$ can be assumed to be a non-increasing sequence, and then the objective function $\|G\|^2$ satisfies

$$\|G\|^2 \geq \sum_{i=1}^{k_0} c_i^4 + \frac{1}{d - k_0} \left(\sum_{i=k_0+1}^n c_i^2 \right)^2. \quad (6)$$

The lower bound of $\|G\|^2$ is achieved if and only if

$$\{g_i\}_{i=1}^n = \{g_i\}_{i=1}^{k_0} \cup \{g_i\}_{i=k_0+1}^n, \quad (7)$$

where $\{g_i\}_{i=1}^{k_0}$ is an orthogonal set, and $\{g_i\}_{i=k_0+1}^n$ forms a regular optimal placement in the $(d - k_0)$ -dimensional orthogonal complement of $\{g_i\}_{i=1}^{k_0}$.

Based on (5) and (7), optimal placements can be analytically constructed. The lower bounds of the objective function $\|G\|^2$ given in (4) and (6) are useful for numerically determining the optimality of a placement. The optimality error defined as the difference between $\|G\|^2$ and its lower bound can be used as a numerical indicator to evaluate the optimality of the placement.

Recall F given in (3) is a function of the sensor-target bearings $\{g_i\}_{i=1}^n$, and irrelevant to the sensor-target ranges $\{\|r_i\|\}_{i=1}^n$. The necessary and sufficient conditions given in Theorems 1 and 2 are the conditions of $\{g_i\}_{i=1}^n$ only. As a result, the sensor-target ranges have no influence on the optimality of a placement. This feature is unique for range-only sensors. For other types of sensors such as bearing-only or received-signal-strength based sensors, the optimal placements will be influenced by sensor-target ranges^[13].

III. AUTONOMOUSLY DEPLOY OPTIMAL SENSOR PLACEMENT

In practical applications, it is usually required to autonomously deploy an optimal sensor placement instead of manually deploying. In this section, we present a control strategy which can steer mobile sensors from an initial non-optimal placement to an optimal one. In the meantime, the control strategy can fulfill given trajectory constraints of the mobile sensors.

A. Control Strategy

The mobile sensors usually cannot move freely in practical applications. For example, the trajectory of each sensor may be constrained on the boundary of a set in \mathbf{R}^d . In order to autonomously deploy an optimal sensor placement, we need to solve two problems: 1) minimize the objective function $\|G\|^2$, and in the meantime 2) fulfill the trajectory constraint of each

mobile sensor. Hence we define two artificial potentials. First, define $V_I = \|G\|^2$ as the inter-sensor potential. The placement is optimal if and only if V_I is minimized. Second, define V_E as the external potential corresponding to the sensor trajectory constraints. The sensor trajectory constraints are fulfilled if and only if $V_E = 0$. By combining the two potentials, we have the total potential as

$$V = k_I V_I + k_E V_E,$$

where $k_I, k_E > 0$. The gradient control law for sensor i is designed as

$$\dot{s}_i = -(k_I \nabla_{s_i} V_I + k_E \nabla_{s_i} V_E), \quad (8)$$

where ∇_{s_i} denotes the gradient with respect to s_i . The target is assumed to be stationary. Hence we have $\nabla_{s_i} V_I = \nabla_{r_i} V_I$ as $r_i = s_i - p$.

B. Inter-sensor Force $\nabla_{s_i} V_I$

Recall $G = \sum_{i=1}^n c_i^2 g_i g_i^T$ and $G^T = G$. Then the differential of V_I is

$$\begin{aligned} dV_I &= 2\text{tr}(GdG) = \\ &= 2\text{tr} \left(G \sum_{i=1}^n c_i^2 dg_i g_i^T \right) + 2\text{tr} \left(G \sum_{i=1}^n c_i^2 g_i dg_i^T \right) = \\ &= 4 \sum_{i=1}^n c_i^2 g_i^T G dg_i. \end{aligned} \quad (9)$$

Furthermore, from $g_i = r_i / \|r_i\|$ we have

$$dg_i = \frac{1}{\|r_i\|} P_i dr_i, \quad (10)$$

where $P_i = I_d - g_i g_i^T \in \mathbf{R}^{d \times d}$ is an orthogonal projection matrix satisfying $P_i^T = P_i$ and $P_i^2 = P_i$. Substituting (10) into (9) yields

$$\nabla_{s_i} V_I = \nabla_{r_i} V_I = \frac{4c_i^2}{\|r_i\|} P_i G g_i. \quad (11)$$

Remark 1. The implementation of (11) requires all-to-all communications among the sensors due to the term G . However, it is possible to implement (11) in a distributed way. To do that, each sensor needs to maintain an estimate \hat{G}_i of G , and \hat{G}_i should converge to G given certain underlying graph. The distributed estimation of G actually is an average consensus problem which has been investigated extensively (see, for example, [16–18]).

C. External Force $\nabla_{s_i} V_E$

The external potential V_E is chosen according to practical application requirements. Here we use two specific scenarios, one of which is 2D and the other is 3D, to demonstrate how control strategy (8) can be applied to practical problems.

1) A 2D scenario

Suppose the sensors can only move on an ellipse, while the stationary target is located arbitrarily inside the ellipse (see Fig. 2). The position of sensor i must satisfy

$$(s_i - s_0)^T Q (s_i - s_0) = 1,$$

where $s_0 \in \mathbf{R}^2$ is the center of the ellipse and $Q = \text{diag}\{1/a^2, 1/b^2\} \in \mathbf{R}^{2 \times 2}$ with $a > 0$ and $b > 0$ as the

lengths of the two semi-axes, respectively. According to the constraint, we choose V_E as

$$V_E = \sum_{i=1}^n [(s_i - s_0)^T Q (s_i - s_0) - 1]^2. \quad (12)$$

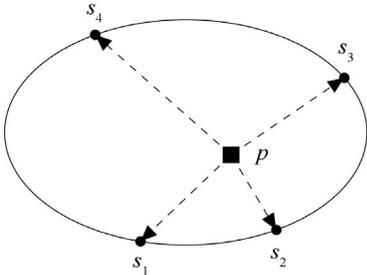


Fig. 2. An illustration of the 2D scenario where all mobile sensors move on an ellipse.

Then it is straightforward to obtain

$$\nabla_{s_i} V_E = 4 [(s_i - s_0)^T Q (s_i - s_0) - 1] Q (s_i - s_0). \quad (13)$$

The implementation of (13) can be distributed because it only requires the information of sensor i . The parameters of the ellipse such as Q and s_0 should be also known by sensor i .

2) A 3D scenario

We now consider a 3D scenario that can be applied to cooperative air and ground surveillance^[12, 19]. Suppose there are multiple unmanned aerial vehicles (UAVs) and unmanned ground vehicles (UGVs). Each vehicle is equipped with a range-only sensor that can measure the range to the target. The UAVs fly at fixed altitudes and the UGVs move on the ground with altitude as zero (see Fig. 3). Denote ℓ_i as the altitude of vehicle i . Then the external potential V_E can be chosen as

$$V_E = \sum_{i=1}^n (e_3^T s_i - \ell_i)^2, \quad (14)$$

where $e_3 = [0, 0, 1]^T \in \mathbf{R}^3$. Clearly, all the altitude constraints are satisfied if and only if $V_E = 0$. It is straightforward to obtain

$$\nabla_{s_i} V_E = 2(e_3^T s_i - \ell_i)e_3. \quad (15)$$

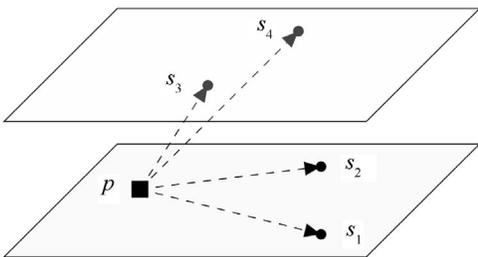


Fig. 3. An illustration of the 3D scenario where each sensor moves at a fixed altitude.

D. Compatibility of V_I and V_E

The proposed gradient control law (8) guarantees that the gradient $k_I \nabla_{s_i} V_I + k_E \nabla_{s_i} V_E$ for all i will converge to zero. However, $k_I \nabla_{s_i} V_I + k_E \nabla_{s_i} V_E = 0$ does not imply

$\nabla_{s_i} V_I = \nabla_{s_i} V_E = 0$. To have that implication, the external potential V_E and the inter-sensor potential V_I should be *compatible* with each other. By compatibility, we mean $k_I \nabla_{s_i} V_I + k_E \nabla_{s_i} V_E = 0$ for all i if and only if $\nabla_{s_i} V_I = \nabla_{s_i} V_E = 0$ for all i . If V_E is not compatible with V_I , it is possible that $k_I \nabla_{s_i} V_I + k_E \nabla_{s_i} V_E = 0$ while $\nabla_{s_i} V_I \neq 0$ and $\nabla_{s_i} V_E \neq 0$.

We next prove $V_I = \|G\|^2$ is compatible with V_E given in (12) or (14). To do that, we will show $\nabla_{s_i} V_I$ in (11) is impossible to be parallel to $\nabla_{s_i} V_E$ in (13) or (15). Firstly consider $\nabla_{s_i} V_I$ in (11). Since $P_i = I_d - g_i g_i^T$, we have $\text{null}(P_i) = \text{span}\{g_i\}$ and hence $P_i r_i = 0$. As a result,

$$r_i^T \nabla_{s_i} V_I = 0,$$

which means $\nabla_{s_i} V_I \perp r_i$. Secondly, consider $\nabla_{s_i} V_E$ given in (13) and (15).

1) In the 2D scenario, vector $\nabla_{s_i} V_E$ is the normal vector of the ellipse at point s_i . Geometrically, it is clear that $\nabla_{s_i} V_E$ is impossible to be orthogonal to r_i for any p inside the ellipse and any s_i on the ellipse. As a result, $\nabla_{s_i} V_E$ is not parallel to $\nabla_{s_i} V_I$, and hence $k_I \nabla_{s_i} V_I + k_E \nabla_{s_i} V_E = 0$ if and only if $\nabla_{s_i} V_I = \nabla_{s_i} V_E = 0$ for all i .

2) In the 3D scenario, vector $\nabla_{s_i} V_E$ is the normal vector of the horizontal planes. Define $\mathcal{I} = \{1, \dots, n\}$, $\mathcal{I}_{>0} = \{i \in \mathcal{I} : \ell_i > 0\}$ and $\mathcal{I}_{=0} = \{i \in \mathcal{I} : \ell_i = 0\}$. Geometrically, it is clear that if $\ell_i > 0$, then $\nabla_{s_i} V_E$ is impossible to be orthogonal to r_i . Hence $\nabla_{s_i} V_E$ is not parallel to $\nabla_{s_i} V_I$ for all $i \in \mathcal{I}_{>0}$. As a result, $k_I \nabla_{s_i} V_I + k_E \nabla_{s_i} V_E = 0$ for all $i \in \mathcal{I}_{>0}$ if and only if $\nabla_{s_i} V_I = \nabla_{s_i} V_E = 0$ for all $i \in \mathcal{I}_{>0}$. Since the inter-sensor forces are mutual, if $\nabla_{s_i} V_I = 0$ for all $i \in \mathcal{I}_{>0}$, then we have $\sum_{i \in \mathcal{I}_{=0}} \nabla_{s_i} V_I = 0$. Furthermore, since r_i for all $i \in \mathcal{I}_{=0}$ is located in the plane with $\ell_i = 0$, we have that $\nabla_{s_i} V_I$ is within the plane and cannot be parallel to $\nabla_{s_i} V_E$. Thus $k_I \nabla_{s_i} V_I + k_E \nabla_{s_i} V_E = 0$ for all $i \in \mathcal{I}_{=0}$ if and only if $\nabla_{s_i} V_I = \nabla_{s_i} V_E = 0$ for all $i \in \mathcal{I}_{=0}$. Therefore, $k_I \nabla_{s_i} V_I + k_E \nabla_{s_i} V_E = 0$ for all $i \in \mathcal{I}$ if and only if $\nabla_{s_i} V_I = \nabla_{s_i} V_E = 0$ for all $i \in \mathcal{I}$.

In fact, if the sensors are constrained on the smooth boundary of an arbitrary convex set in \mathbf{R}^d and the target is located inside the convex set, the norm vector $\nabla_{s_i} V_E$ is impossible to be parallel to $\nabla_{s_i} V_I$. Hence the corresponding V_E will always be compatible with $V_I = \|G\|^2$. We only consider the case that sensors are constrained on the boundary of a set in this paper. But more complicated issues such as obstacle avoidance and collision avoidance among sensors could also be solved by introducing more external potentials. At last, it should be noted that the compatibility of V_I and V_E does not guarantee that the final converged placement is optimal. That is because $\nabla_{s_i} V_I = 0$ for all i is only necessary but not sufficient for a placement to be optimal. This point has been discussed in [13].

IV. SIMULATIONS

We next present simulation results to verify the proposed control strategy for the 2D and 3D scenarios. We first consider two scenarios with static targets, then we consider a scenario with a dynamic target. It is assumed that the sensor networks have all-to-all communications.

A. Autonomous Sensor Deployment for Static Targets

1) *2D scenario*: In the 2D scenario, all sensors are constrained on an ellipse while the target is located inside the ellipse. The external force $\nabla_{s_i} V_E$ is given in (13). The standard deviations of the sensor noises are assumed to be one, i.e., $\sigma_i = 1$ for all i . Note the final optimal placement is determined only by the relative values of $\{\sigma_i\}_{i=1}^n$ but not the absolute values. As shown in Fig. 4, given appropriate initial placements, the control strategy can steer sensors to optimal placements while ensuring the sensor trajectory constraints fulfilled. The optimality error shown in Fig. 4 refers to the difference between the objective function $\|G\|^2$ and its lower bound given in (4) or (6). As can be seen, the control strategy can efficiently reduce the optimality errors to zero.

Numerically, it is clear that the final placements in Fig. 4 are optimal because the optimality errors converge to zero. We next analytically determine the optimality of the final placements based on the analytical results presented in [13]. As shown in Fig. 4(a), the angle subtended by the two sensors in the final placement is 90 deg. Hence we have $g_1 \perp g_2$ in the final placement. Then the final placement is optimal by [13, Theorem 4.4]. As shown in Fig. 4(b), the sensors are steered to equally spaced angular positions around the target. The angle subtended by any two sensors in the final placement is 120 deg. This kind of equally spaced angular placements

are optimal as concluded in [13, Section 5.2]. At the first glance, it is intuitively unclear whether the final placement in Fig. 4(c) is optimal. The final placement of the four sensors can be viewed as a combination of two sub-placements: the sub-placement of sensors 1 and 3, and the one of sensors 2 and 4. Note the angle subtended by sensors 1 and 3 and the one by sensors 2 and 4 are both 90 deg in the final placement. That means $g_1 \perp g_3$ and $g_2 \perp g_4$, and the two sub-placements are (regular) optimal, respectively. By [13, Theorem 5.6], the final placement in Fig. 4(c) is optimal.

2) *3D scenario*: In the 3D scenario, it is assumed that each sensor is carried by a UAV or UGV that moves at a fixed altitude. The standard deviations of the sensor noises are assumed to be one, i.e., $\sigma_i = 1$ for all i . Simulation results with $n = 3$ and 4 are respectively shown in Figs. 5(a) and 5(b). As shown in Fig. 5, the optimality errors in the two cases are both reduced to zero efficiently.

In Fig. 5(a), the angle subtended by any two sensors is 90 deg in the final placement. That means $g_1, g_2,$ and g_3 are mutually orthogonal in the final placement. By [13, Theorem 4.4], the final placement is optimal. The final optimal placement shown in Fig. 5(b) actually is the one given in [13, Fig. 7(c)]. In both cases of $n = 3$ and $n = 4$, the final converged placements are optimal and the sensor position constraints are simultaneously fulfilled.

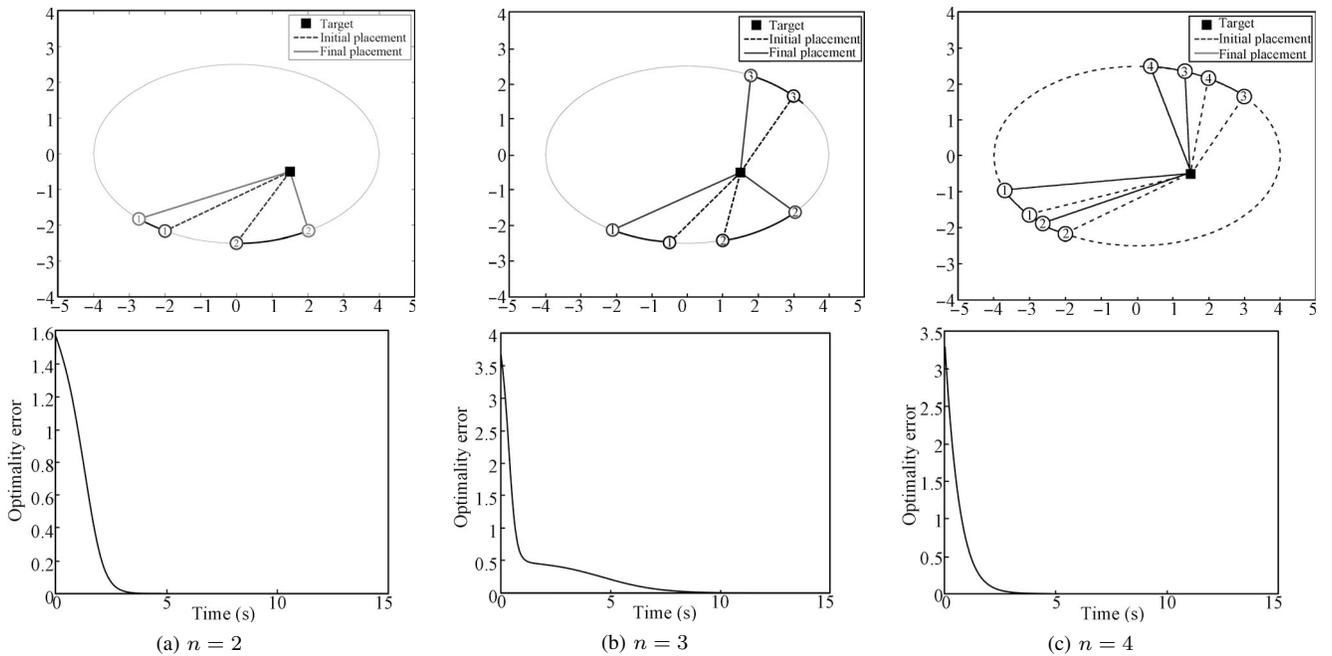
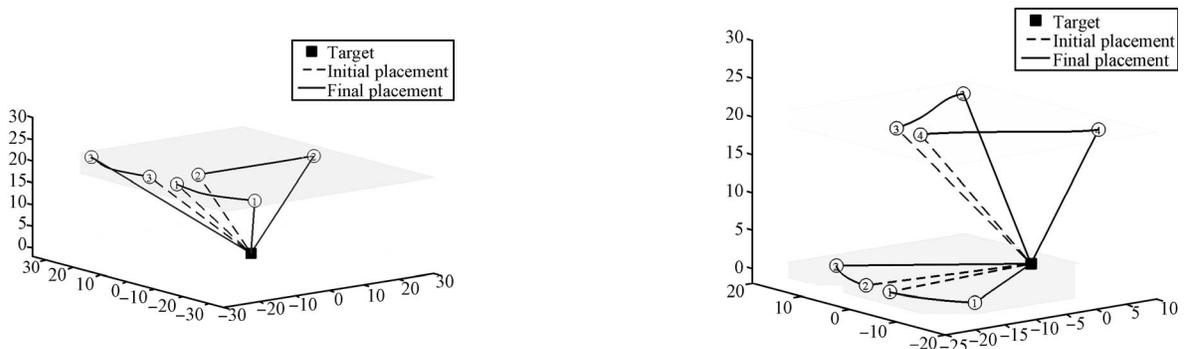


Fig. 4. Sensor trajectories and optimality errors for the 2D scenario.



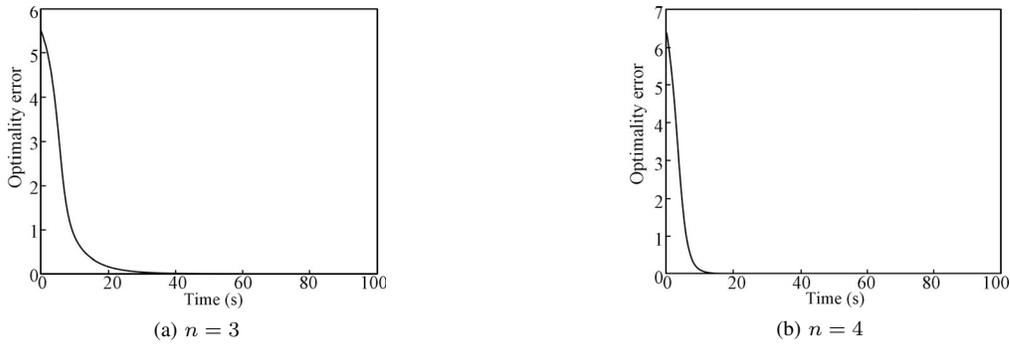


Fig. 5. Sensor trajectories and optimality errors for the 3D scenario.

B. Autonomous Sensor Deployment for Dynamic Targets

Although it is assumed that the target is stationary, the proposed control strategy can also be applied to tracking of a dynamic target in practice. We next consider a 3D cooperative target tracking scenario. Suppose there are three UAVs flying at the same altitude. Each UAV carries a range-only sensor to measure the distance to the ground target. In the simulation, the target moves on a non-flat ground. The 3D maneuvering motion of the target is given as

$$p(t) = \begin{bmatrix} 0.5t \\ 10 \sin(\frac{\pi}{5}t) \\ 3 - 3 \cos(\frac{\pi}{20}t) \end{bmatrix}.$$

See Fig. 6 for the target trajectory.

In this cooperative target tracking scenario, all UAVs need to share their range measurements to estimate the target position, and move to form an optimal placement in the meantime. The autonomous optimal sensor deployment algorithm is summarized as Algorithm 1.

Algorithm 1. Autonomous optimal sensor deployment for target tracking

Step 1. Obtain an initial estimate of the target position $\hat{p}(0)$.

Step 2. At time t , estimate the target position $\hat{p}(t)$ using a centralized extended Kalman filter (EKF). The EKF is established based on the following process and measurement models:

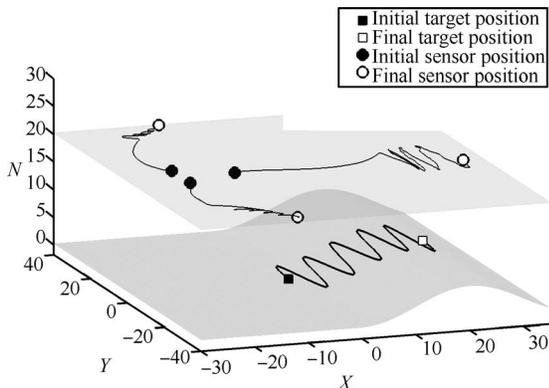


Fig. 6. Autonomous optimal sensor deployment to track a dynamic target (The target moves on the non-flat ground and the three UAVs fly at a fixed altitude.)

$$\begin{aligned} \dot{p} &= v, \\ m_i &= \|p - s_i\| + w_i, \quad i = 1, \dots, n, \end{aligned}$$

where $m_i \in \mathbf{R}$ is the measurement of sensor i , and $v \in \mathbf{R}^3$ and $w_i \in \mathbf{R}$ for all i are white Gaussian noises.

Step 3. Based on $\hat{p}(t)$, autonomously deploy the optimal sensor placement using the control strategy (8).

Step 4. At time $t + 1$, go to Step 2.

The real initial position of the target is $p(0) = [0, 0, 0]^T$, while the initial target estimate for the EKF is $\hat{p}(0) = [-4, 5, 3]^T$. The standard deviation of noise w_i is set as three meters. By Algorithm 1, the trajectories of the three moving sensors are obtained as shown in Fig. 7. The behaviors of the three sensors in Fig. 7 can be explained as the following: the three sensors attempt to form a placement where each angle subtended at the target by any two sensors is 90 deg. In order to illustrate how optimal placements can improve the target tracking performance, we compare the target estimation results in the cases of moving and stationary sensors. In the case of stationary sensors, the three sensors stay statically at the initial placement shown in Fig. 7. The initial placement is obviously not optimal. The target estimation results in the two cases are shown in Fig. 7. As can be seen, the target can be tracked accurately when the sensors are steered to maintain an optimal placement, while the tracking performance is worse when the sensors are stationary. Note the parameters of the EKF are the same in the two cases.

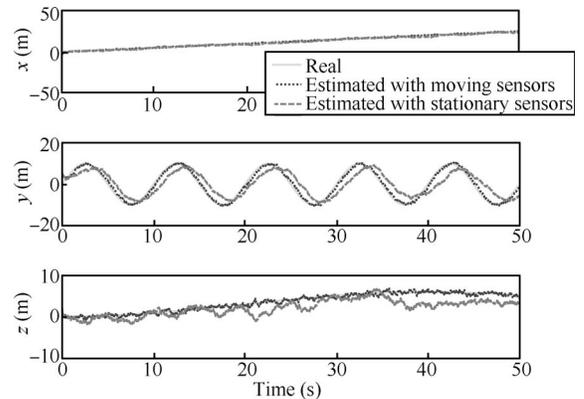


Fig. 7. Target position estimation results by stationary and moving sensors.)

V. CONCLUSIONS

Based on the results in [13], this work presented a flexible control strategy for autonomously deploying optimal placements of range-only sensors for target tracking. Two practical scenarios were considered and solved using the proposed control strategy. The control strategy was also applied to a 3D cooperative target tracking scenario. It was shown that the

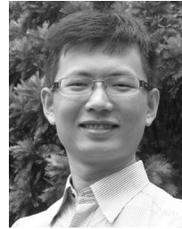
target tracking performance can be improved when sensors are steered to maintain an optimal placement.

There are several directions for future research. First, this paper only considers the cases of all-to-all communications. Distributed autonomous deployment, distributed target tracking and the integration of them need to be investigated in the future. Second, this paper only considers homogenous sensor networks but not heterogeneous cases^[20]. Cooperative target tracking using heterogeneous sensor networks is a practically important topic for future research.

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